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**UTILITY  
PATENT APPLICATION  
TRANSMITTAL**

(Only for new nonprovisional applications under 37 CFR 1.53(b))

Attorney Docket No.

ARNEY 8-51-1

First Inventor

Susanne Arney

Title

OXIDATION SENSOR FOR AN ELECTRICAL CIRCUIT AND A METHOD OF  
MANUFACTURE THEREFOR

Express Mail Label No.

**APPLICATION ELEMENTS**

See MPEP chapter 600 concerning utility patent application contents.

ADDRESS TO:

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1. ☒ Fee Transmittal Form (e.g., PTO/SB/17)  
(Submit an original and a duplicate for fee processing)
2. ☐ Applicant claims small entity status.  
See 37 CFR 1.27.
3. ☒ Specification [ Total Pages  ]  
(preferred arrangement set forth below)
- Descriptive title of the invention
  - Cross Reference to Related Applications
  - Statement Regarding Fed sponsored R & D
  - Reference to sequence listing, a table,  
or a computer program listing appendix
  - Background of the Invention
  - Brief Summary of the Invention
  - Brief Description of the Drawings ( if filed )
  - Detailed Description
  - Claim(s)
  - Abstract of the Disclosure
4. ☒ Drawing(s) (35 U.S.C. 113) [ Total Sheets  ]
5. Oath or Declaration [ Total Pages  ]
- a. ☐ Newly executed (original or copy)
- b. ☐ Copy from a prior application (37 CFR 1.63 (d))  
(for continuation/divisional with Box 17 completed)
- i. ☐ **DELETION OF INVENTOR(S)**  
Signed statement attached deleting inventor(s)  
named in the prior application, see 37 CFR  
1.63(d)(2) and 1.33(b).
6. ☐ Application Data Sheet. See 37 CFR 1.76

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- a. ☐ Computer Readable Form (CRF)
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**ACCOMPANYING APPLICATION PARTS**

9. ☐ Assignment Papers (cover sheet & document(s))
10. ☐ 37 CFR 3.73(b) Statement [ ☐ Power of  
(when there is an assignee) Attorney
11. ☐ English Translation Document (if applicable)
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Prior application information:

Examiner .....

Group / Art Unit. ....

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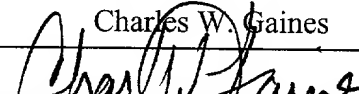
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36,804

Signature



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Jc946 U.S. PTO

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# FEE TRANSMITTAL for FY 2000

Patent fees are subject to annual revision.

TOTAL AMOUNT OF PAYMENT (\$ ) 1,124.00

## Complete if Known

Application Number	N/A
Filing Date	Herewith
First Named Inventor	Susanne Arney
Examiner Name	N/A
Group Art Unit	N/A
Attorney Docket No.	ARNEY 8-51-1

Jc921 US PTO  
09/27/00

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Deposit Account Name	Lucent Technologies

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☐ Applicant claims small entity status See 37 CFR 1.27

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## FEE CALCULATION

## 1. BASIC FILING FEE

Large Entity Fee Code (\$)	Small Entity Fee Code (\$)	Fee Description	Fee Paid
101 710	201 355	Utility filing fee	710.00
106 320	206 160	Design filing fee	
107 490	207 245	Plant filing fee	
108 710	208 355	Reissue filing fee	
114 150	214 75	Provisional filing fee	

SUBTOTAL (1) (\$ ) 710.00

## 2. EXTRA CLAIM FEES

Total Claims	Extra Claims	Fee from below	Fee Paid
43	-20** = 23	18.00	414.00
3	-3** = 0	80.00	0.00
Multiple Dependent			

\*\*or number previously paid, if greater; For Reissues, see below

## Large Entity Small Entity

Fee Code (\$)	Fee Code (\$)	Fee Description
103 18	203 9	Claims in excess of 20
102 80	202 40	Independent claims in excess of 3
104 270	204 135	Multiple dependent claim, if not paid
109 80	209 40	** Reissue independent claims over original patent
110 18	210 9	** Reissue claims in excess of 20 and over original patent

SUBTOTAL (2) (\$ ) 414.00

## FEE CALCULATION (continued)

## 3. ADDITIONAL FEES

Large Entity Fee Code (\$)	Small Entity Fee Code (\$)	Fee Description	Fee Paid
105 130	205 65	Surcharge - late filing fee or oath	
127 50	227 25	Surcharge - late provisional filing fee or cover sheet	
139 130	139 130	Non-English specification	
147 2,520	147 2,520	For filing a request for ex parte reexamination	
112 920*	112 920*	Requesting publication of SIR prior to Examiner action	
113 1,840*	113 1,840*	Requesting publication of SIR after Examiner action	
115 110	215 55	Extension for reply within first month	
116 390	216 195	Extension for reply within second month	
117 890	217 445	Extension for reply within third month	
118 1,390	218 695	Extension for reply within fourth month	
128 1,890	228 945	Extension for reply within fifth month	
119 310	219 155	Notice of Appeal	
120 310	220 155	Filing a brief in support of an appeal	
121 270	221 135	Request for oral hearing	
138 1,510	138 1,510	Petition to institute a public use proceeding	
140 110	240 55	Petition to revive - unavoidable	
141 1,240	241 620	Petition to revive - unintentional	
142 1,240	242 620	Utility issue fee (or reissue)	
143 440	243 220	Design issue fee	
144 600	244 300	Plant issue fee	
122 130	122 130	Petitions to the Commissioner	
123 50	123 50	Petitions related to provisional applications	
126 240	126 240	Submission of Information Disclosure Stmt	
581 40	581 40	Recording each patent assignment per property (times number of properties)	
146 710	246 355	Filing a submission after final rejection (37 CFR § 1.129(a))	
149 710	249 355	For each additional invention to be examined (37 CFR § 1.129(b))	
179 710	279 355	Request for Continued Examination (RCE)	
169 900	169 900	Request for expedited examination of a design application	

Other fee (specify) \_\_\_\_\_

\* Reduced by Basic Filing Fee Paid

SUBTOTAL (3) (\$ ) 0.00

## SUBMITTED BY

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**OXIDATION SENSOR FOR AN ELECTRICAL CIRCUIT AND A  
METHOD OF MANUFACTURE THEREFOR**

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# OXIDATION SENSOR FOR AN ELECTRICAL CIRCUIT AND A METHOD OF MANUFACTURE THEREFOR

## TECHNICAL FIELD OF THE INVENTION

The present invention is directed, in general, to an oxidation  
5 sensor for an electrical circuit and, more specifically, to a  
system to provide early warning of oxidation of surface micro-  
machined Poly-Si MEMS structures.

## BACKGROUND OF THE INVENTION

Micro-electromechanical systems (MEMS) is a well known  
10 technology that combines microfabricated electrical circuits with  
microfabricated mechanical devices such as sensors, valves, gears,  
mirrors and actuators fabricated on or in semiconductor chips, and  
is an industry that is growing at an accelerating pace. A MEMS  
15 device contains micro-circuitry on a tiny silicon chip into which  
a mechanical device such as a mirror has been manufactured. The  
mechanical device moves mechanically under the control of an  
electrical signal or the device is externally activated and the  
motion is detected electrically or optically. MEMS systems include  
20 systems such as spatial light modulators, deformable mirrors,  
steerable mirrors, shutters, micro-antennas, relays, and  
accelerometers. With the rapid commercialization of MEMS, their  
reliability is of great importance.

In the area of unpassivated MEMS devices, it is recognized that humidity can be an accelerating factor for most phenomena that may detrimentally affect the devices. Because there is no protective covering on top of the poly-silicon electrodes and wires, they are packaged absolutely hermetically in order to protect the devices from unknown reliability issues.

To prevent the detrimental effects associated with humidity, the industry has designed various packaging systems to isolate the MEMS device from the humidity as much as possible. For example, the industry has developed hermetically sealed ceramic packages that contain the MEMS chip.

In some cases, the hermetically sealed ceramic package can become cracked or damaged sufficiently to allow moisture to enter the package. In such cases, the ingress of moisture within the package can result in operational failure of the device. Moisture may also come from sources inside the package, such as epoxies. The most well known failure phenomenon is stiction, which is the strong interfacial adhesion present between contacting surfaces.

Another failure phenomenon associated with humidity in MEMS devices is oxidation in mechanical systems. If microcracks exist in a system where there is a mechanical device made of silicon, a bit of native oxide can form inside the crack due to the presence of oxygen or water. Any kind of native oxidation, even at the Angstrom or nanometer level will cause a volume expansion inside

the crack, which helps to drive the crack further and further into the silicon. The crack can not be closed because the oxide takes up twice the volume of the silicon it consumed. For these reasons, oxidation of silicon can contribute to mechanical reliability issues. This phenomenon has been demonstrated in fracture and fatigue of silicon parts.

Another problem associated with humidity is the reduction of the reflective coefficient of the metals used in optical MEMS devices. The mirrors used in optical MEMS devices are typically made up of a material that reflects light with high reflectivity at the desired wavelength of the light, for example at about the 1000 - 1600 nm wavelength range for the silicon dioxide optical fiber-based telecommunication systems. Some examples of such reflective materials are gold, silver, rhodium, platinum, copper or aluminum. These reflective metal films are deposited on a movable membrane substrate such as a silicon substrate. Optically, if you have a metal that is subject to tarnishing, then oxidation or moisture can lead to reducing the reflective coefficient of the metal. The reduction of the reflective coefficient of the metal in turn results in the inability to operate the device at its optimum capacity.

Accordingly, what is needed in the art is a system to provide early warning of system failure of polysilicon structures, thereby allowing the operator to replace the leaky package before device

failure due to humidity-induced failure phenomena.

1. The first failure mode is the failure of the material due to the humidity-induced failure phenomena.

## SUMMARY OF THE INVENTION

To address the above-discussed deficiencies of the prior art, the present invention provides an oxidation sensor for an electrical circuit or MEMS device that includes a conductor located on an insulating substrate and a sensor trace located on the insulating substrate adjacent the conductor. The sensor trace is located on the insulating substrate adjacent the conductor and is configured to oxidize at a rate greater than an electrical component that is associated with the sensor trace when the sensor trace and the electrical component are exposed to a same oxidizing environment. By oxidizing and thus becoming an open circuit more rapidly than any structure on a chip at a given relative humidity, the oxidation sensor is designed to provide early warning of oxidation. Thus, the present invention serves as a sensor that will give advance warning of a leaky or outgassing package and associated oxidation.

The foregoing has outlined, rather broadly, preferred and alternative features of the present invention so that those skilled in the art may better understand the detailed description of the invention that follows. Additional features of the invention will be described hereinafter that form the subject of the claims of the invention. Those skilled in the art should appreciate that they can readily use the disclosed conception and specific embodiment as



a basis for designing or modifying other structures for carrying out the same purposes of the present invention. Those skilled in the art should also realize that such equivalent constructions do not depart from the spirit and scope of the invention in its  
5      broadest form.

## BRIEF DESCRIPTION OF THE DRAWINGS

For a more complete understanding of the present invention, reference is now made to the following descriptions taken in conjunction with the accompanying drawings, in which:

5       FIGURE 1A illustrates a top view of an oxidation sensor of the present invention;

FIGURE 1B illustrates a top view of a chip containing several sub-chips, 4 of which contain oxidation sensors;

10       FIGURE 2A is a plot of an oxidation sensor's resistance vs. time for 7 oxidation sensors of the present invention under different relative humidities;

15       FIGURE 2B is a table of the time to fully oxidize an oxidation sensor of the present invention at 110 Volts for several relative humidities;

20       FIGURE 3 graphically illustrates data regarding the amount of oxidation of a polysilicon sensor trace at various relative humidities and differing voltages;

FIGURE 4 illustrates a top view of one configuration of the present invention in which many 90° bends are constructed into the sensor trace;

FIGURE 5 illustrates three example structures that the oxidation sensor of the present invention may assume;

FIGURE 6 illustrates a sectional view of the tunnel structure

that the oxidation sensor of the present invention may assume where the oxidation sensor is capped by a grounded roof of poly-silicon;

FIGURE 7 illustrates a top view of an unused sensor trace and conductors;

5           FIGURE 8 illustrates a top view of an oxidized sensor trace 101 after 4 hours at 60% RH and +110V;

FIGURE 9 is a top view of a non-tunnel, style A oxidation sensor illustrating a connector being used to connect the grounded conductor to a ground contact via; and

10           FIGURE 10 illustrates one way that the sensor trace may be electrically connected so that it anodically oxidizes.

## DETAILED DESCRIPTION

Referring to Figure 1A, illustrated is a top view of an oxidation sensor 100 for an electrical circuit, such as one that might be associated with an micro-electromechanical system (MEMS), constructed according to the principles of the present invention, which includes conductors 102 located on an insulating substrate and a sensor trace 101 located on the insulating substrate adjacent the conductor 102. An electrical component 103 will typically be associated with the sensor trace 101. For example, the electrical component 103 may be a conductive trace in adjacent electrical circuits or MEMS devices located on the same circuit board, chip or on another chip in the same package. An electrical component 103 is associated with the sensor trace 101 when the electrical component 103 is, for example, located within the same package, such that oxidation of the sensor trace 101 gives advanced warning of oxidation of the electrical component 103. In a broader sense, it should be understood that the electrical component 103 may be any electrical component or device that is associated with the sensor circuit 101 that is susceptible to oxidation when subjected to the substantially the same environment as the sensor trace 101, such that oxidation of the sensor trace 101 gives advanced warning of oxidation of the electrical component 103. An exemplary embodiment which illustrates one such association is shown in FIGURE 1B, where the electrical component 103 may be any component

on the same circuit board or within the same package. FIGURE 1B illustrates 4 subchips 101b that are located within a chip 100b. Within subchips 101b, there may be any number of oxidation sensors 100. For example, with respect to a MEMS device, there may be several MEMS chips and only one oxidation sensor 100, or one MEMS chip and several oxidation sensors 100 in a package.

In an advantageous embodiment, the sensor trace 101 is located between the conductors 102, and when in the presence of an applied voltage, the sensor trace 101 has a positive potential that is greater than a potential of the conductor 102. The sensor trace 101 is configured, as explained below, to oxidize at a rate greater than the electrical components 103 on adjacent electrical circuits or MEMS devices when exposed to the same oxidizing environment. In one advantageous embodiment, the sensor trace 101 comprises silicon because of its electrical and mechanical properties as well as its relative ease of processing in devices such as surface micromachined MEMS. The sensor trace 101 may comprise a conductive material selected from a number of conductive materials including titanium, copper, tungsten, aluminum, and tantalum. In one advantageous embodiment, the sensor trace 101 has a serpentine configuration, which allows the sensor trace 101 to have as long a length as possible, given design and restricted space parameters. A longer sensor trace 101 makes for a more sensitive sensor trace 101 with respect to oxidation.

As discussed previously, the MEMS chip typically consists of mechanical components and electrical circuits or wires. One common material for the wires is unpassivated poly-silicon. The MEMS chip normally operates in an ultra-dry ambient in a hermetically sealed package. In the case where a MEMS chip package is no longer hermetic as a result of moisture ingress or outgassing of moisture in the package, several failure phenomena may result. As discussed previously, stiction and oxide growth in microcracks are two failure phenomena associated with humidity.

However, another problem, which has previously been unrecognized for MEMS devices is anodic oxidation of electrical components in the MEMS device, which in itself may be a failure phenomenon if it is left to transpire in the package for a long period of time. Anodic oxidation has recently been found to occur when moisture is present and there is a finite leakage current between neighboring poly-silicon electrodes or wires held at different electrical potential on the surface of the insulator. While the anodic oxidation was recently reported on polysilicon traces, it can also occur on any oxidizable conductor, such as aluminum, copper, etc. As the silicon is oxidized, it changes from conductive poly-silicon to insulating silicon oxide. That is, more and more conductive wire is replaced by insulating silicon dioxide. When the insulating silicon dioxide consumes the entire wire, then it becomes an insulator entirely. In other words, if the silicon

is anodically oxidized long enough, the silicon ceases to be a conductor and becomes an open circuit. Once a wire becomes an open circuit, the electrode it drives becomes non-functional. Anodic oxidation of wires and electrodes can eventually lead to open circuits, as well as to gradual changes in the capacitance between electrical structures. Consequently, if moisture is introduced into the system the MEMS chip can eventually fail either from anodic oxidation of the wires and electrodes, or from other failure phenomena such as stiction and oxide growth. Thus, it is advantageous to have the sensor trace 101 present on the MEMS chip or on another chip in the same package so that early detection of oxidation can be achieved.

As previously mentioned and as discussed below, the sensor trace 101 is configured to oxidize more rapidly than the electrical component 103 on a MEMS chip in the same package. This oxidation can occur when moisture is present around the device. Moreover, any oxidation that is present within the device can be accelerated by a current that flows between the sensor trace 101 and the conductors 102, when sensor trace 101 is held at a more positive potential than conductor 102. As current flows, it leads to oxidation of the sensor trace 101, which can be detected by using an ohmmeter to measure the change in resistance of the sensor trace 101. As the sensor trace 101 oxidizes, its resistivity increases and eventually the sensor trace 101 is fully oxidized and the

resistance jumps to a substantially higher resistance value.

In an exemplary embodiment, the sensor trace 101 may be narrow enough that partially oxidizing it substantially compromises its resistive or capacitive properties. The more narrower sensor trace 101 is, the more sensitive to oxidation it is. The state of the art for polysilicon wires used in MEMS devices is 1-2 microns. Thus, in a preferred embodiment, the device of the present invention will be oxidized most effectively if the sensor trace 101 is less than 2 microns in width. Although the sensor trace 101 is configured less than 2 microns in width in a preferred embodiment, it should be recognized that the sensor trace 101 may be configured at any width so long as it overall physical design allows it to oxidize prior to other wires in the system, thereby providing an early detection of package leakage.

The gap 104 between the sensor trace 101 and the conductor 102 may also affect the rate of oxidation, as it affects both the leakage current and the electric field (for a fixed potential drop between electrodes). For example, in one embodiment, the gap between the sensor trace 101 and the conductor 102 may be about 2  $\mu\text{m}$  or less. However, a narrower gap 104 may operate to accelerate the rate of oxidation. Although FIGURE 1A illustrates that the gap 104 is measured adjacent to the conductor 102, it should be noted that the gap 104 may also be measured vertically to another electrode or wire.



The oxidation sensor 100 may further include bonds pads 105 that can be connected to the sensor trace 101. While FIGURE 1A illustrates the bond pads 105 connected directly to the sensor trace 101 with the electrical component 103, the bond pads 105 may also be connected to the sensor trace 101. One bond pad may be used to keep the sensor trace 101 at an elevated positive potential with respect to the conductor 102. A second bond pad may be used in conjunction with the first pad to measure resistance of the sensor trace 101. The bond pads 105 may be made of any conductive material.

In one exemplary embodiment, the conductor 102 is grounded; however, it is not necessary for purposes of the present invention that the conductor 102 be grounded in order that the sensor trace 101 oxidize before other wires or electrodes in the system. The sensor trace 101 is preferably configured to have a positive potential greater than a potential of the conductor 102 when a voltage is applied to the oxidation sensor 100. In such embodiments, as long as the conductor 102 is negative with respect to the sensor trace 101, the absolute potential of the conductor 102 does not matter.

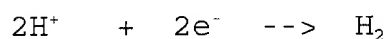
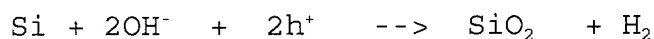
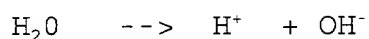
In a particularly advantageous embodiment, the conductor 102 and the sensor trace 101 as illustrated in FIGURE 1A are unpassivated. Because passivation inhibits oxidation, the sensor trace 101 and the conductor 102 are unpassivated in order to

effectively oxidize. If the hermetic package within which the chip and oxidation sensor 100 are sealed were to leak, the resistance of sensor trace 101 would increase and be measured by the oxidation sensor 100 long before the electrical circuit or MEMS device itself would oxidize to the point of affecting performance or other failure phenomena begin to occur in the system. While the sensor trace 101 and the conductor 102 are unpassivated in advantageous embodiments, it should be noted that, unlike the sensor trace 101 and the conductor 102, the electrical component 103 may be passivated.

In environments with high voltage as well as high humidity, oxidation of poly-silicon wires and electrodes is especially observed. In one embodiment of the present invention, the oxidizing environment of the oxidation sensor 100 includes a relative humidity of greater than 50% and voltages of greater than 10 volts. When the MEMS chip is operated in these conditions, the most positively biased electrodes oxidize. While exemplary embodiments include a relative humidity of greater than 50% and voltages of greater than 10 volts, it should be recognized that other conditions of relative humidity and voltage that can cause an oxidizing environment are also included in the scope of the present invention.

It has been observed that relative humidity is an accelerating factor in the oxidation of the sensor trace 101 because the higher

the humidity, the more water is absorbed on the insulation substrate between sensor trace 101 and conductor 102, which facilitates oxidation of the sensor trace 101. It is believed that the decomposition of water takes place and forms OH radicals that react with silicon in the presence of electrons and holes to form silicon oxide. The reaction governing anodic oxidation is:



As can be seen from the equation, only the positively biased electrode (supplying holes, labeled h) is oxidized, while the negatively biased electrode (supplying electrons, e) is unaffected. It is clear, at least from the above theoretical reaction equations, why the oxidation occurs at the positive electrode.

The effects of the presence of humidity within these devices is demonstrated in FIGURE 2A. FIGURE 2A is a plot of an oxidation sensor's resistance vs. time for 7 oxidation sensors constructed in accordance with the principles of the present invention under different relative humidities (RH). Two oxidation sensors are operated under 51% RH (204), two under 63% RH (203), two under 68% RH (202), and one oxidation sensor is operated under 83% RH (201). When humidity is present, the resistance increases over a period of time, and as shown in FIGURE 2B, the higher the humidity, the quicker the complete oxidation of the sensor trace 101 and, thus,

the time to open circuit. As illustrated in FIGURE 2A, at 51% RH (204), the resistance does not increase over the test period, while at the higher humidities, the oxidation sensor becomes open circuits within hours. As noted in Figure 2B, it takes more than 48 hours for an oxidation sensor at 51% RH to become an open circuit. On the other hand, it takes only 0.9 hours for an oxidation sensor at 83% RH to become an open circuit.

FIGURE 3 graphically illustrates data regarding the amount of oxidation of a polysilicon sensor trace after a 24 hour test at various relative humidities and differing voltages. As illustrated in FIGURE 3, at a relative humidity of less than 50%, there is no measurable oxidation. However, at a relative humidity of 65%, the amount of oxidation begins to increase, and at a relative humidity of 79%, the amount of oxidation increases dramatically.

Turning now to FIGURE 4, one advantageous embodiment of a serpentine configuration of the sensor trace 101 is illustrated. In this particular embodiment, the sensor trace 101 has a plurality of angled bends. The angled bends in the sensor trace 101 enhance the rate of oxidation, thereby providing a sensor trace that will oxidize even more rapidly than the other wires in the device. While the angled bends in FIGURE 4 are 90°C, it should be understood that the angles of the sensor trace 101 may range from about 25° to about 175°. Although the most effective oxidation occurs in angles of 175°, a serpentine configuration of the sensor

trace 101 that includes a pattern of angles of around 90° may be used because the oxidation sensor is more easily manufactured when the sensor trace 101 is shaped into 90° angles. While preferred embodiments include angles in the sensor trace 101, it should be understood that the sensor trace need not include angles in order to serve the purpose of sensing oxidation. For example, the sensor trace 101 may be configured in a straight line such as the sensor trace illustrated in FIGURE 1A. Other alternative configurations are shown in FIGURE 5.

The structure illustrated in 503, which includes a number of 90° angles, is an effective oxidation sensor. The angles that are included into the sensor trace 101 operate to sharpen the field lines and accelerate oxidation. The serpentine configurations of 502 and 501 are also effective oxidation sensors. In structure 501, both the sensor trace 101 and conductors 102 assume a serpentine configuration. In structure 502, the sensor trace 101 assumes a serpentine configuration while the conductor 102 assumes a straight configuration along the sensor trace 101. Thus, the sensor trace 101 may be shaped into any number of geometries and still be within the scope of the present invention.

FIGURE 6 illustrates yet another structure that the oxidation sensor 100 may assume. FIGURE 6 illustrates a cross section of the tunnel oxidation sensor. The sensor trace 603 and the conductor 602 are capped by a roof layer 601. In an advantageous embodiment,

the roof layer is a grounded roof layer of polysilicon. As previously mentioned, the width of the sensor trace 606 and the width of the space between the sensor trace 603 and the conductor 602 may be narrow in order to facilitate oxidation. Beneath the sensor trace 603 and conductor 602 is a bottom layer 604. Any generic insulator may be used to construct the bottom layer 604. For example, silicon nitride may be included in the bottom layer 604. In another advantageous embodiment, the height 608 of the grounded roof of polysilicon 601 is as close to the sensor trace 603 as possible, which facilitates oxidation. It should be noted that there are a number of types of different tunnel oxidation sensors that may be configured by adjusting the height 608 of the grounded roof of polysilicon 601 in relation to the sensor trace 603, as well as adjusting other parameters of the tunnel oxidation sensor. The order in which the structures of Figure 5 become open circuits for given relative humidities and bias voltages (and thus serve as more effective oxidation sensors) is 503 of Figure 5, the tunnel structure of Figure 6, 502 of Figure 5 and 501 of Figure 5.

Turning now to FIGURES 7 and 8, illustrated is the effects of anodic oxidation on oxidation sensor 100. FIGURE 7 is a top view of an unused sensor trace 101 and conductors 102. In comparison, FIGURE 8 is an image of the sensor trace 101 and conductors 102 after 4 hours at 60% RH and +110 Volts. As illustrated in FIGURE

8, the sensor trace 101 is very oxidized indicated by areas 101, while the grounded conductors 102 are substantially unoxidized. Due to the amount of oxidation, the sensor trace 101 in FIGURE 8 is electrically an open circuit.

FIGURE 9 is a top view of the configuration 503 illustrated in FIGURE 5. A connector 901 is used to connect the grounded conductor 102 to the ground contact via 902. The sensor trace 101 is connected to the bond pads 105. While FIGURE 9 illustrates a connector 901 that is used to connect the grounded conductor 102 to the ground contact via 902, the connector 901 is not necessary to connect the oxidation sensor system. For example, the grounded conductor 102 may be connected to the ground contact via 902 directly.

FIGURE 10 simply illustrates an advantageous electrical configuration in which the present invention may be incorporated. The potential drop to drive the possible anodic oxidation of the oxidation sensor 100 is supplied by a dc voltage supply 1002. As the oxidation sensor anodically oxidizes, the resistance of the wire increases, and this increase is readily measured using a floating ohmmeter 1001. While the package may be initially hermetically sealed, if the seal is broken and the internal wiring is exposed to moisture, the resistance of the sensor trace rises with time. This advanced warning allows the user to know the package has a problem well before the occurrence of failure

phenomena, such as stiction or oxide growth, which cause failure in the system (for example, in a MEMS device, the moving parts can no longer be made to move). The resistance of the oxidation sensor 100 provides a direct measure of the amount of sensor trace 101 that has been anodically oxidized. An ac monitoring system can also be used to measure the resistance of the sensor trace using a small ac probe voltage while the large dc voltage is still applied to one side of the sensor trace. While an ac monitoring system may be used to measure the resistance of the sensor trace, it should be understood that any voltage measuring technique of sufficient sensitivity can be used to measure the changes in system's resistance or voltage. For example, the user may also measure the current flowing from the sensor trace 101 to the surrounding conductors 102 and use that as an indirect measure of how much oxidation has occurred.

It should be understood that there can be any number of sub-chips of oxidation sensors included in a chip. Moreover, there can be any number of different oxidation sensor combinations of the non-tunnel configurations of FIGURE 5 and the tunnel configuration of FIGURE 6.

Although the present invention has been described in detail, those skilled in the art should understand that they can make various changes, substitutions and alterations herein without departing from the spirit and scope of the invention in its



broadest form.

WHAT IS CLAIMED IS:

1. An oxidation sensor for an electrical circuit,  
comprising:

a conductor located on an insulating substrate; and  
a sensor trace located on the insulating substrate adjacent  
the conductor and configured to oxidize at a rate greater than an  
electrical component associated with the sensor trace when the  
sensor trace and the electrical component are exposed to a same  
oxidizing environment.

2. The oxidation sensor as recited in Claim 1 wherein the  
sensor trace is configured to have a positive potential greater  
than a potential of the conductor in the presence of an applied  
voltage.

3. The oxidation sensor as recited in Claim 1 wherein the  
sensor trace is located a distance from the conductor of about 2  $\mu\text{m}$   
or less.

4. The oxidation sensor as recited in Claim 1 wherein the  
conductor is a grounded conductor.

5. The oxidation sensor as recited in Claim 1 wherein the

2 sensor trace comprises a conductive material selected from the  
3 group consisting of:

4 titanium,  
5 copper,  
6 tungsten,  
7 aluminum, and  
8 tantalum

9 6. The oxidation sensor as recited in Claim 1 wherein the  
10 sensor trace comprises silicon.

7. The oxidation sensor as recited in Claim 1 further  
including bonds pads connected to the sensor trace.

8. The oxidation sensor as recited in Claim 1 wherein the  
sensor trace has a serpentine configuration.

9. The oxidation sensor as recited in Claim 9 wherein the  
serpentine configuration includes a pattern of angles.

10. The oxidation sensor as recited in Claim 10 wherein the  
angles range from about 25 degrees to about 175 degrees.

11. The oxidation sensor as recited in Claim 1 wherein the

2 sensor trace and conductor have a serpentine configuration.

12. The oxidation sensor as recited in Claim 1 wherein the  
2 oxidation sensor is capped by a grounded roof layer.

13. The oxidation sensor as recited in Claim 1 wherein the  
2 sensor trace is unpassivated.

14. The oxidation sensor as recited in Claim 1 wherein the  
2 oxidizing environment includes a relative humidity of greater than  
50% and voltages of greater than 10 volts.

15. The oxidation sensor as recited in Claim 1 wherein the  
sensor trace has a width less than 2 microns.

16. A method of manufacturing an oxidation sensor for an electrical circuit, comprising:

forming a conductor on insulating substrate; and  
forming a sensor trace located on the insulating substrate adjacent the conductor and configured to oxidize at a rate greater than an electrical component associated with the sensor trace and the electrical component are exposed to a same oxidizing environment.

17. The method as recited in Claim 16 wherein forming the sensor trace includes forming the sensor trace so that the sensor trace is configured to have a positive potential greater than a potential of the conductor in the presence of an applied voltage.

18. The method as recited in Claim 16 wherein forming the sensor trace includes forming the sensor trace so that the sensor trace is located at a distance from the conductor of about 2  $\mu\text{m}$  or less.

17. The method as recited in Claim 16 wherein forming the conductor includes forming a grounded conductor.

18. The method as recited in Claim 16 wherein forming the

2 sensor trace includes forming the sensor trace so that the sensor  
3 trace comprises a conductive material selected from the group  
4 consisting of:

5 titanium,  
6 copper,  
7 tungsten,  
8 aluminum, and  
9 tantalum.

19. The method as recited in Claim 16 wherein forming the  
sensor trace includes forming the sensor trace so that the sensor  
trace comprises silicon.

20. The method as recited in Claim 16 wherein forming a  
sensor trace includes forming bonds pads connected to the sensor  
trace.

21. The method as recited in Claim 16 wherein forming the  
sensor trace includes forming the sensor trace with a serpentine  
configuration.

22. The method as recited in Claim 21 wherein forming the  
sensor trace with a serpentine configuration includes forming a  
pattern of angles.

23. The method as recited in Claim 22 wherein forming a  
pattern of angles includes forming a pattern of angles so that the  
angles range from about 25 degrees to about 175 degrees.

24. The method as recited in Claim 16 wherein forming the  
sensor trace and conductor include forming the sensor trace and  
conductor include forming them into a serpentine configuration.

25. The method as recited in Claim 16 wherein forming the  
the oxidation sensor includes forming the oxidation sensor such  
that it is capped by a grounded roof layer.

26. The method as recited in Claim 16 wherein forming the  
sensor trace includes forming an unpassivated sensor trace.

27. The method as recited in Claim 16 wherein exposing the  
sensor trace and the electrical component to an oxidizing  
environment includes a relative humidity of greater than 50% and  
voltages of greater than 10 volts.

28. The method as recited in Claim 16 wherein forming the  
sensor trace includes forming the sensor trace such that a width of  
the sensor trace is less than 2 microns.

29. A micro-electromechanical device, comprising:

an actuator;

an actuation mechanism;

an electrical component; and

an oxidation sensor, comprising:

a conductor located on an insulating substrate; and

a sensor trace located on the insulating substrate adjacent the conductor and configured to oxidize at a rate greater than the electrical component trace when the sensor trace and the electrical component are exposed to a same oxidizing environment.

30. The oxidation sensor as recited in Claim 29 wherein the sensor trace is configured to have a positive potential greater than a potential of the conductor in the presence of an applied voltage.

31. The oxidation sensor as recited in Claim 29 wherein the sensor trace is located a distance from the conductor of about 2  $\mu\text{m}$  or less.

32. The oxidation sensor as recited in Claim 29 wherein the conductor is a grounded conductor.

33. The oxidation sensor as recited in Claim 29 wherein the



2 sensor trace comprises a conductive material selected from the  
3 group consisting of:

4 titanium,

5 copper,

6 tungsten,

7 aluminum, and

8 tantalum.

34. The oxidation sensor as recited in Claim 29 wherein the  
2 sensor trace comprises silicon.

35. The oxidation sensor as recited in Claim 29 further  
2 including bonds pads connected to the sensor trace.

36. The oxidation sensor as recited in Claim 29 wherein the  
2 sensor trace has a serpentine configuration.

37. The oxidation sensor as recited in Claim 36 wherein the  
2 serpentine configuration includes a pattern of angles.

38. The oxidation sensor as recited in Claim 37 wherein the  
2 angles range from about 25 degrees to about 175 degrees.

39. The oxidation sensor as recited in Claim 29 wherein the

2 sensor trace and conductor have a serpentine configuration.

40. The oxidation sensor as recited in Claim 29 wherein the  
2 oxidation sensor is capped by a grounded roof layer.

41. The oxidation sensor as recited in Claim 29 wherein the  
2 electrical component and the sensor trace are unpassivated.

42. The oxidation sensor as recited in Claim 29 wherein the  
2 oxidizing environment includes a relative humidity of greater than  
50% and voltages of greater than 10 volts.

43. The oxidation sensor as recited in Claim 29 wherein the  
sensor trace has a width less than 2 microns.

OXIDATION SENSOR FOR AN ELECTRICAL CIRCUIT AND A  
METHOD OF MANUFACTURE THEREFOR

ABSTRACT OF THE DISCLOSURE

5 The present invention provides an oxidation sensor for an  
electrical circuit or MEMS device that includes a conductor located  
on an insulating substrate and a sensor trace located on the  
insulating substrate adjacent the conductor. The sensor trace is  
located on the insulating substrate adjacent the conductor and is  
configured to oxidize at a rate greater than an electrical  
10 component associated with the sensor trace on the electrical  
circuit or MEMS device when the sensor trace and the electrical  
component are exposed to a same oxidizing environment. By  
oxidizing and thus becoming an open circuit more rapidly than any  
structure on a electrical circuit or MEMS device at a given  
15 relative humidity (i.e. in the same package), the oxidation sensor  
is designed to provide early warning of oxidation. Thus, the  
present invention serves as a sensor that will give advance warning  
of a leaky package and associated oxidation.

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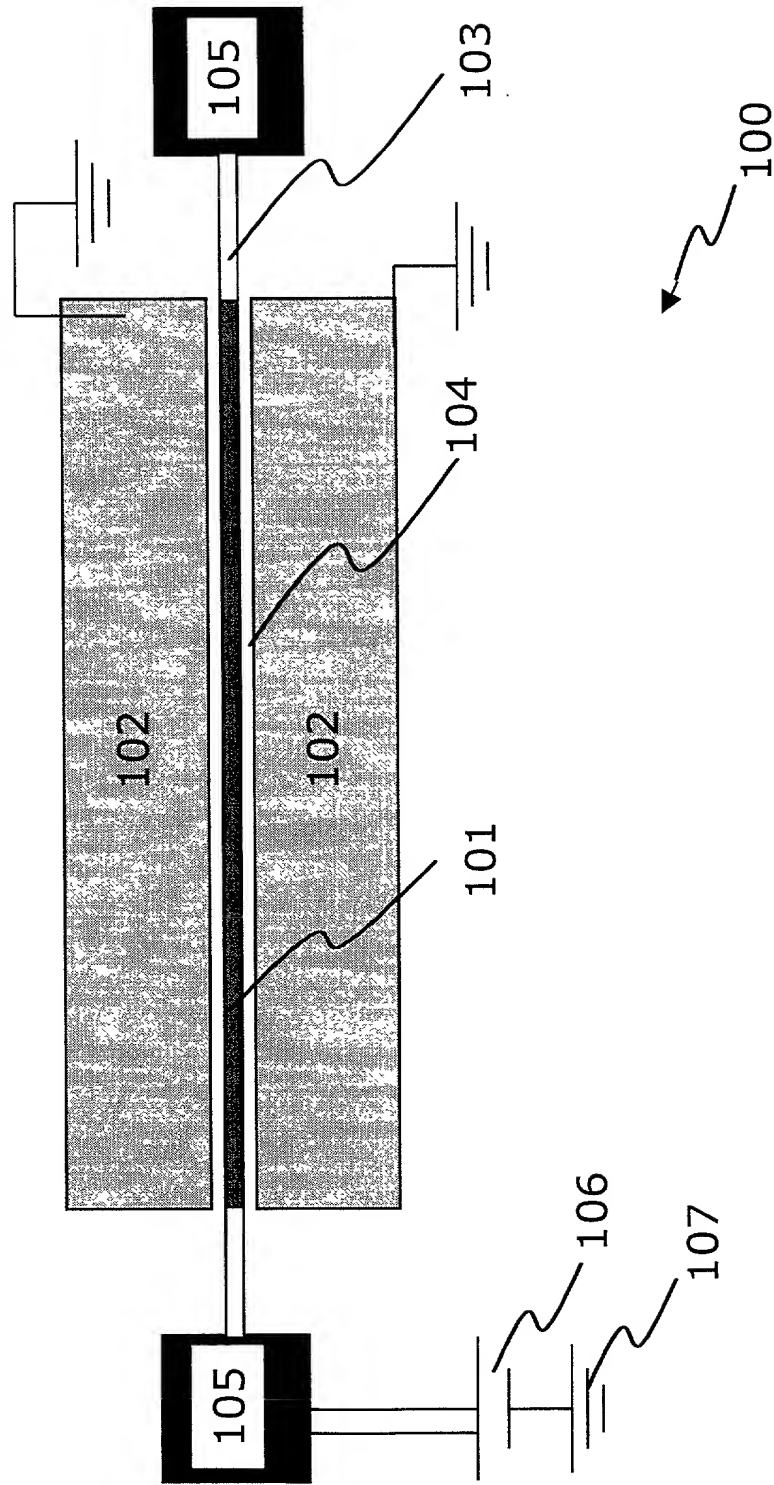


FIGURE 1A

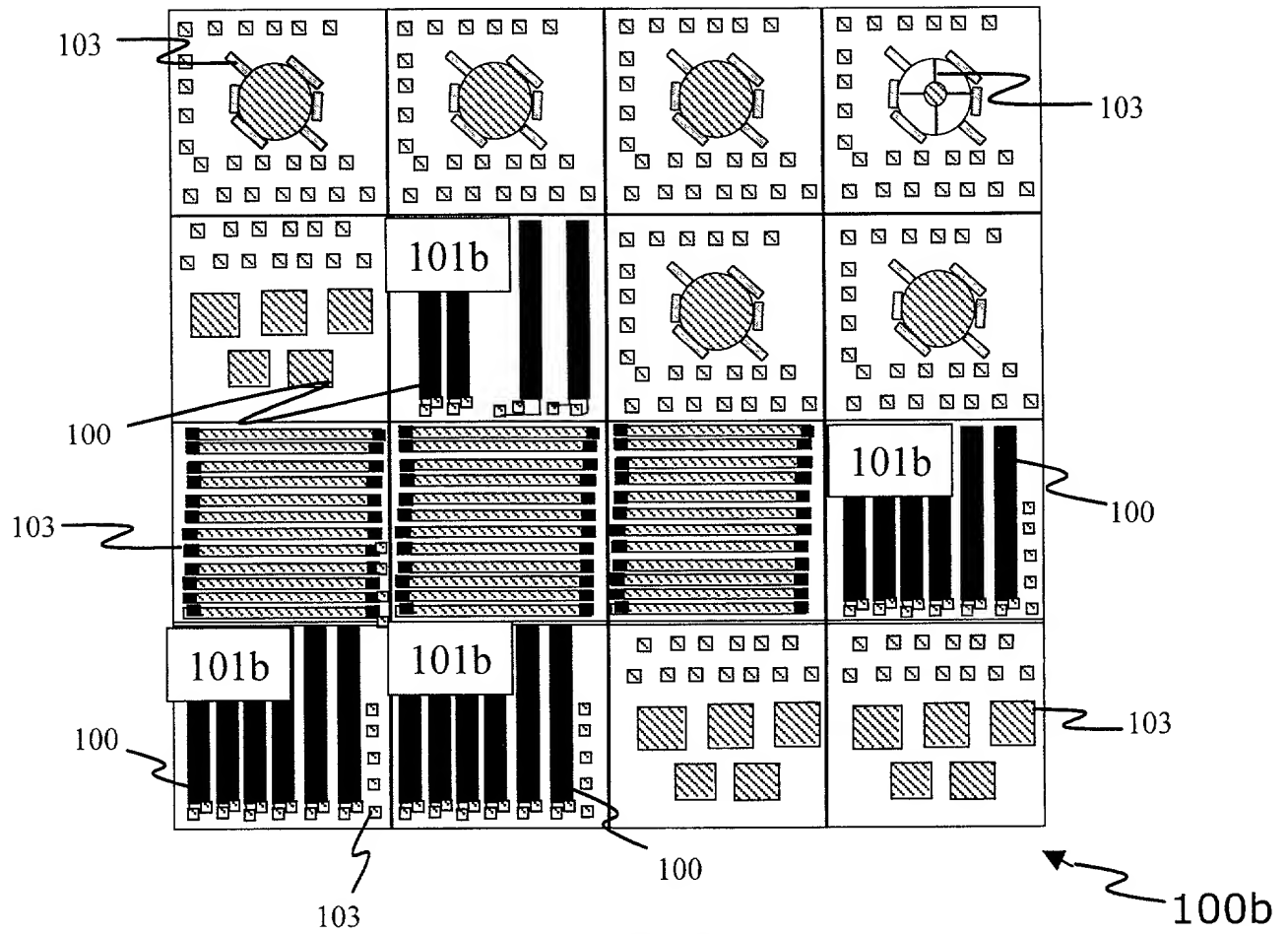


FIGURE 1B

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FIGURE 2A

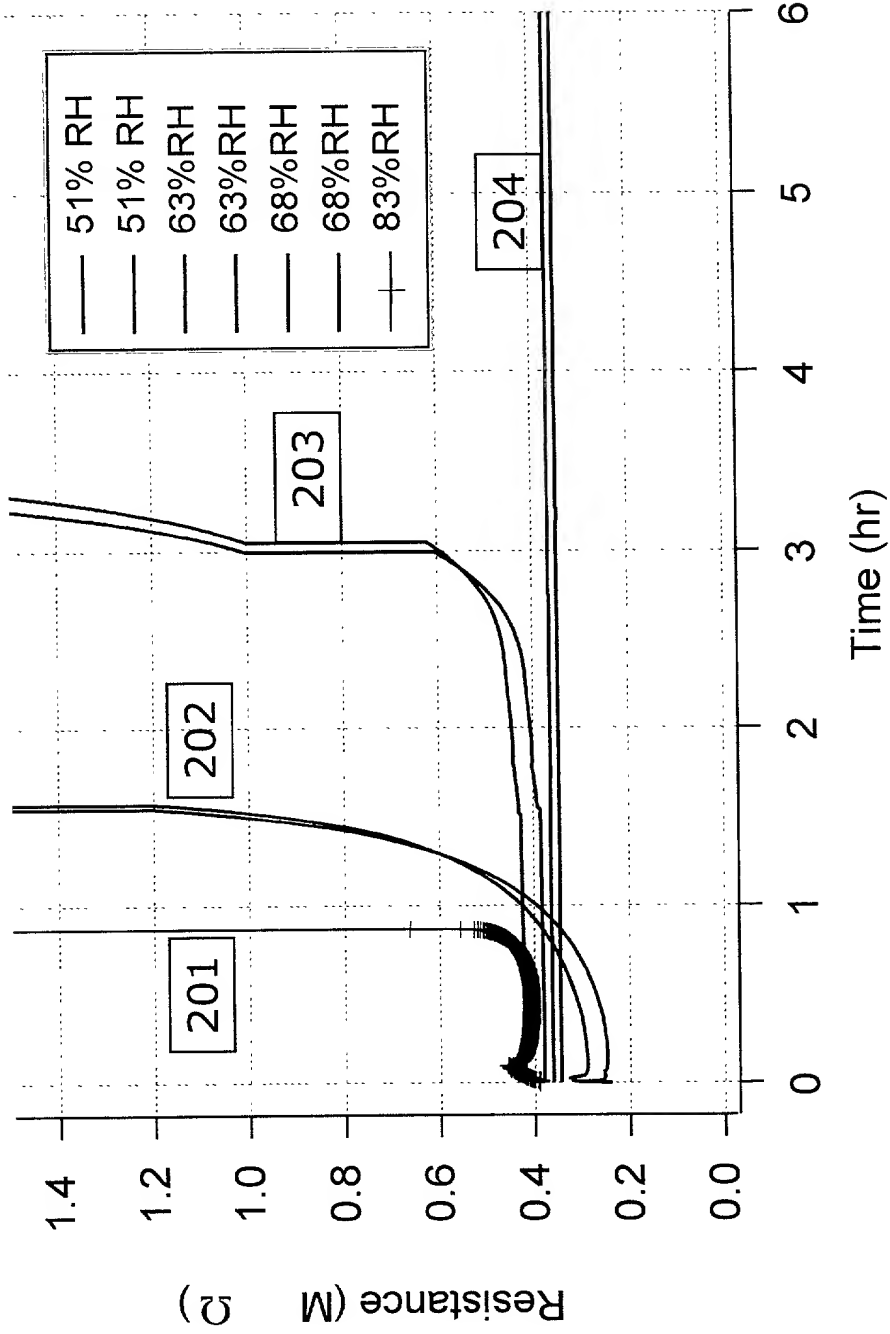


FIGURE 2B

%RH	51	63	68	83
Time to open Circuit (hours)	>48	3.5	1.5	0.9

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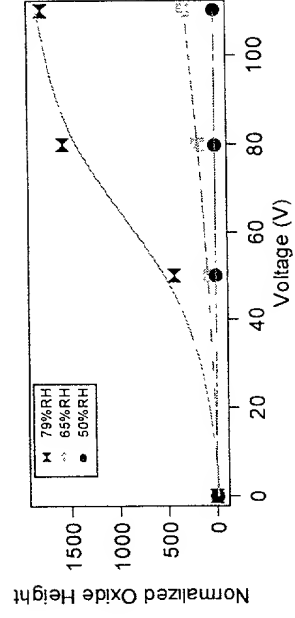


FIGURE 3

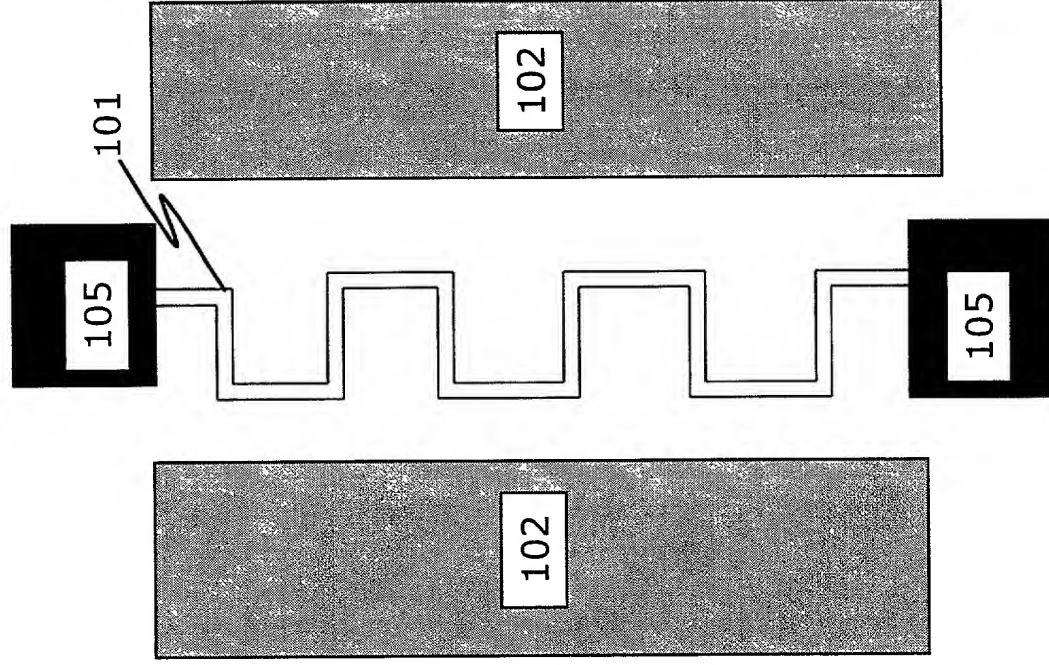


FIGURE 4



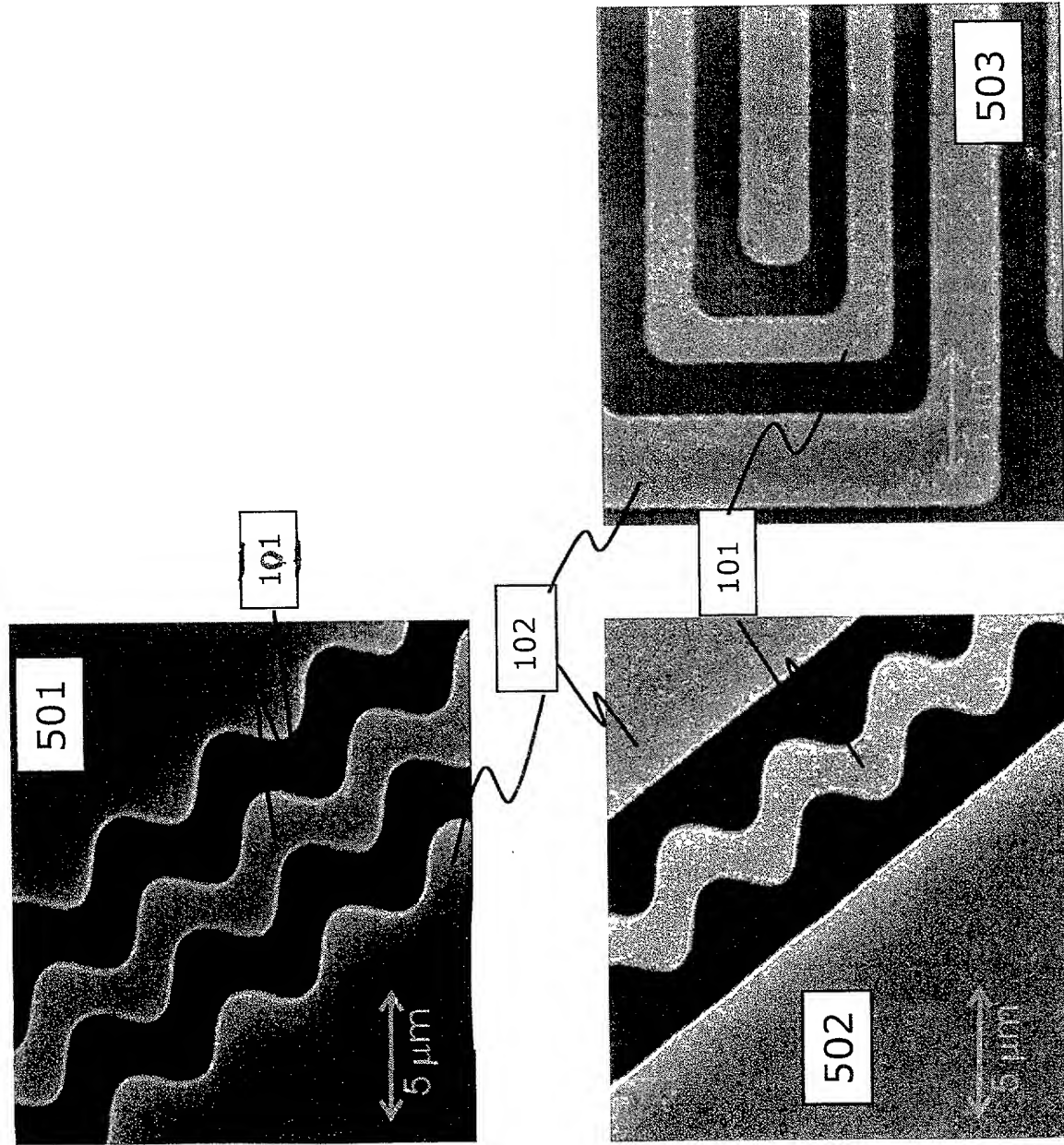


FIGURE 5

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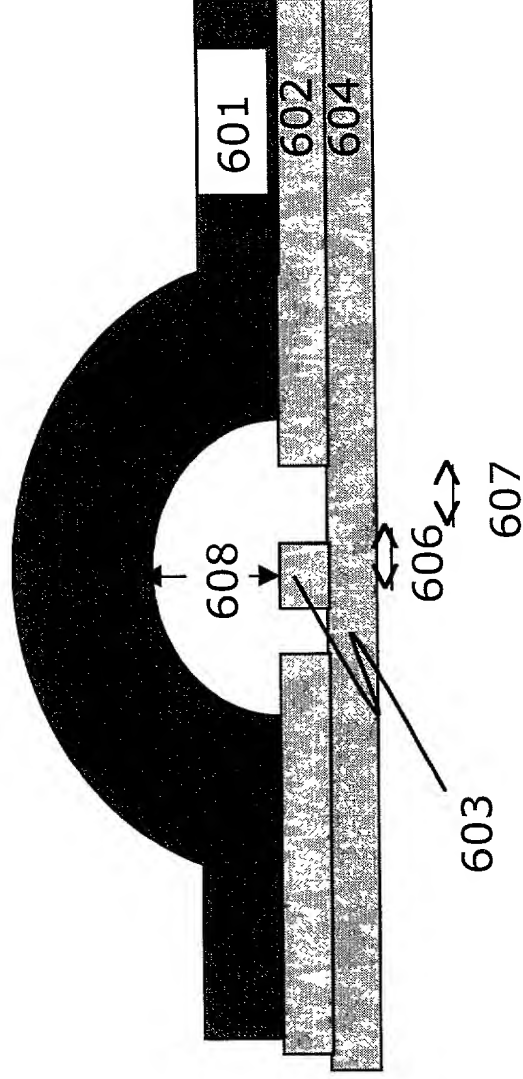


FIGURE 6

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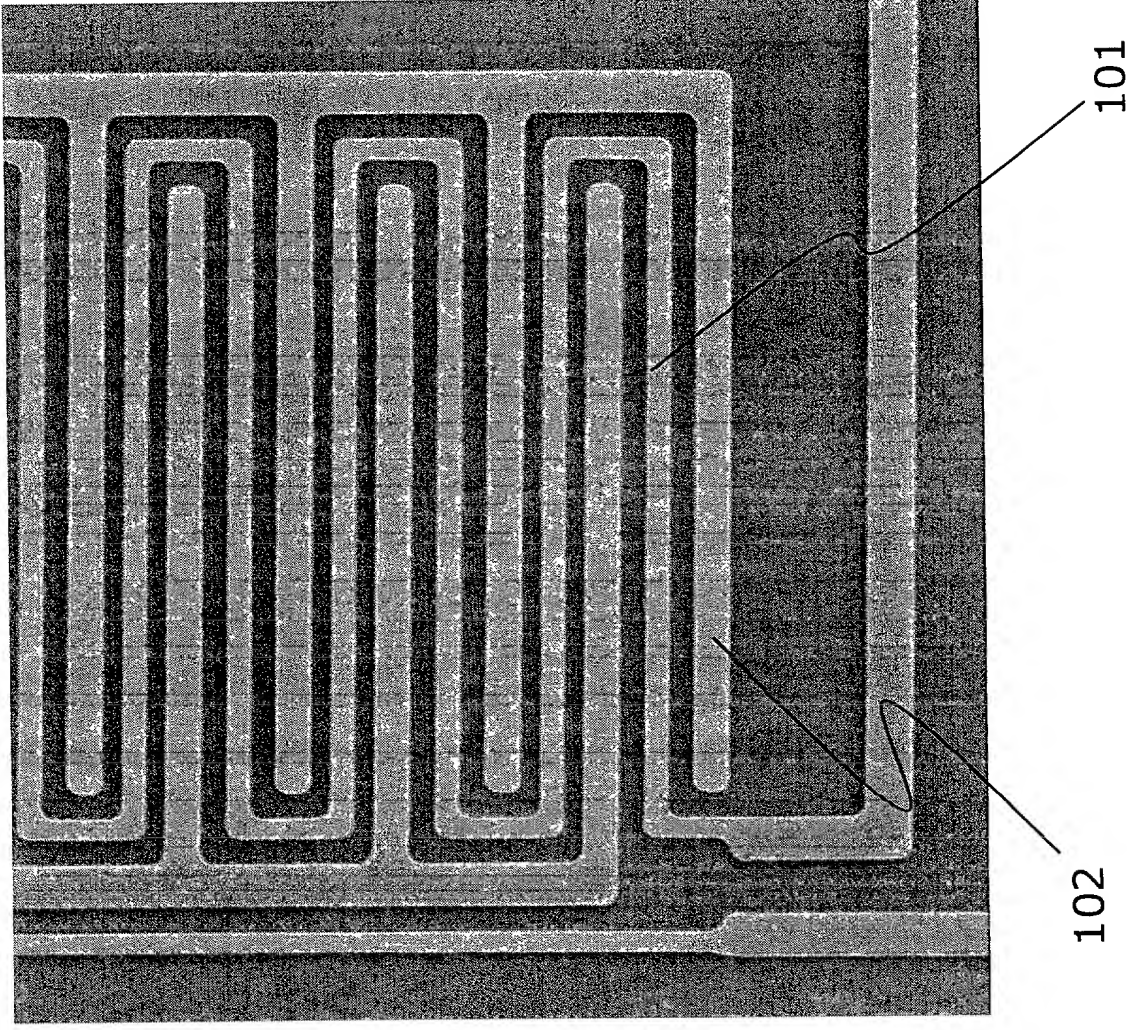


FIGURE 7

Patented Apr. 14, 1992

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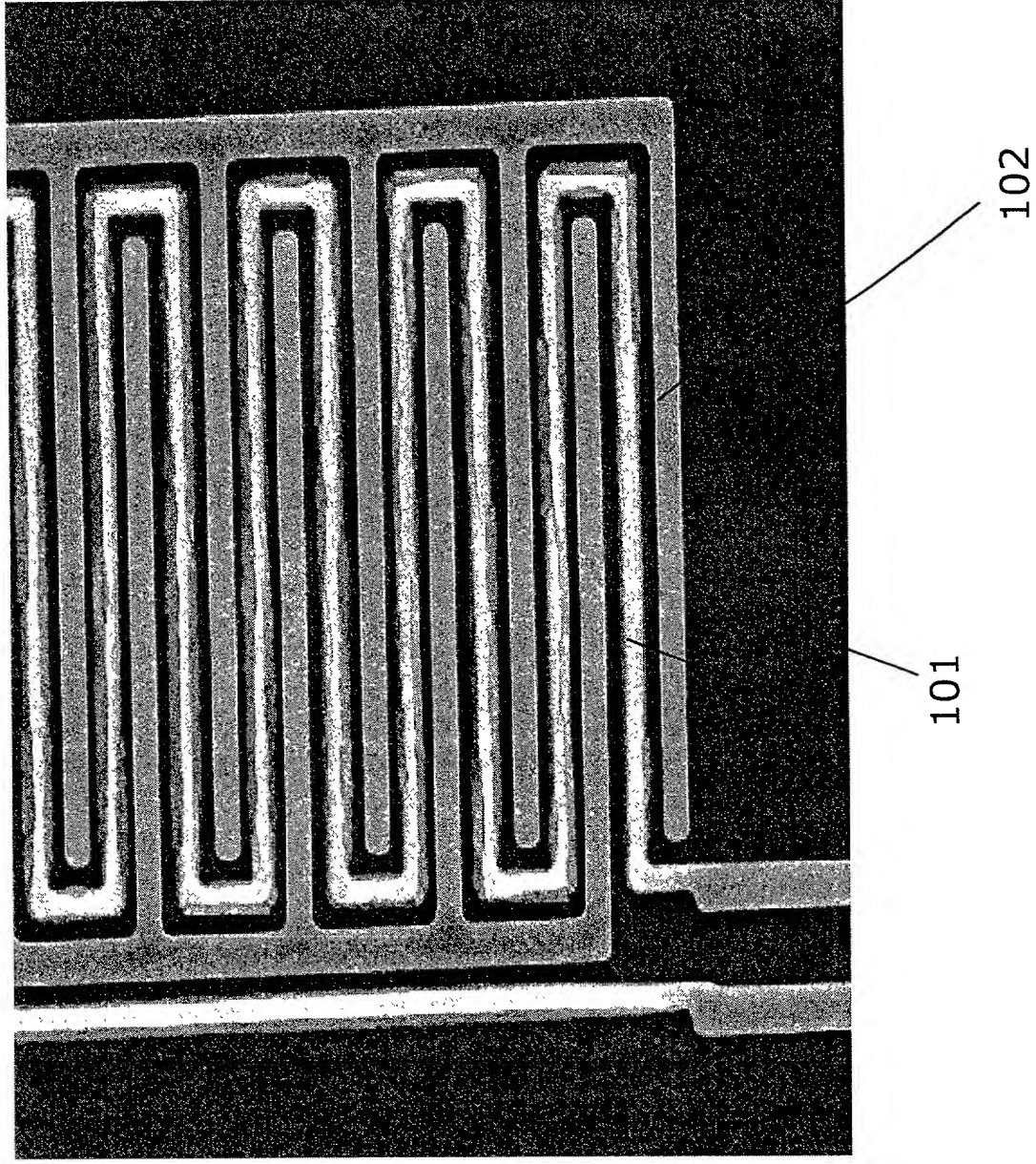


FIGURE 8

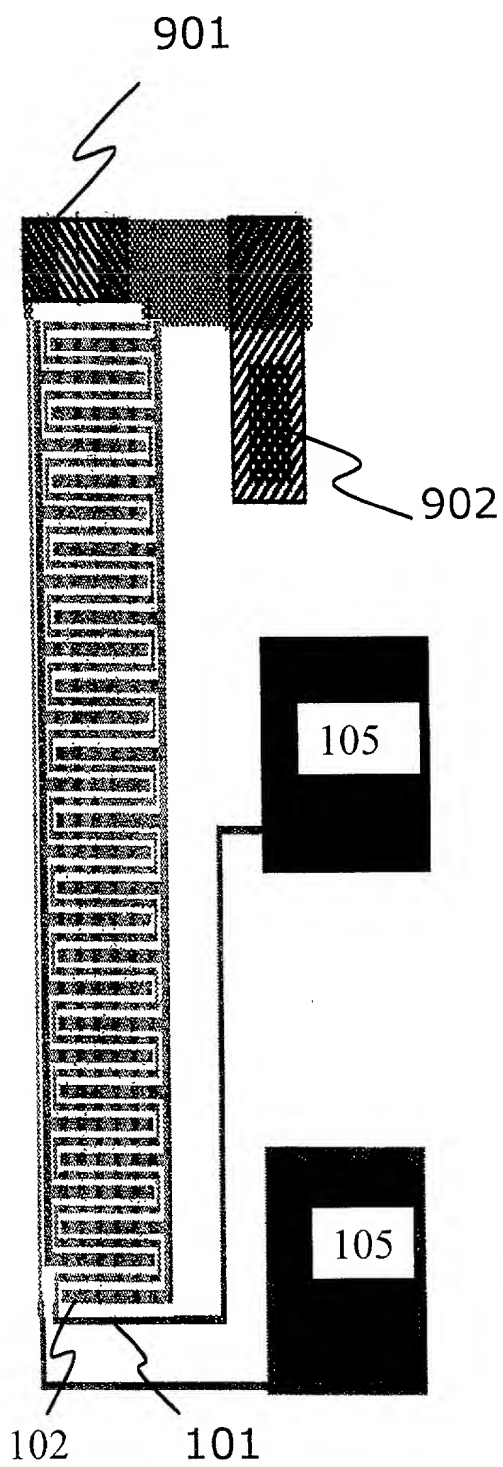


FIGURE 9

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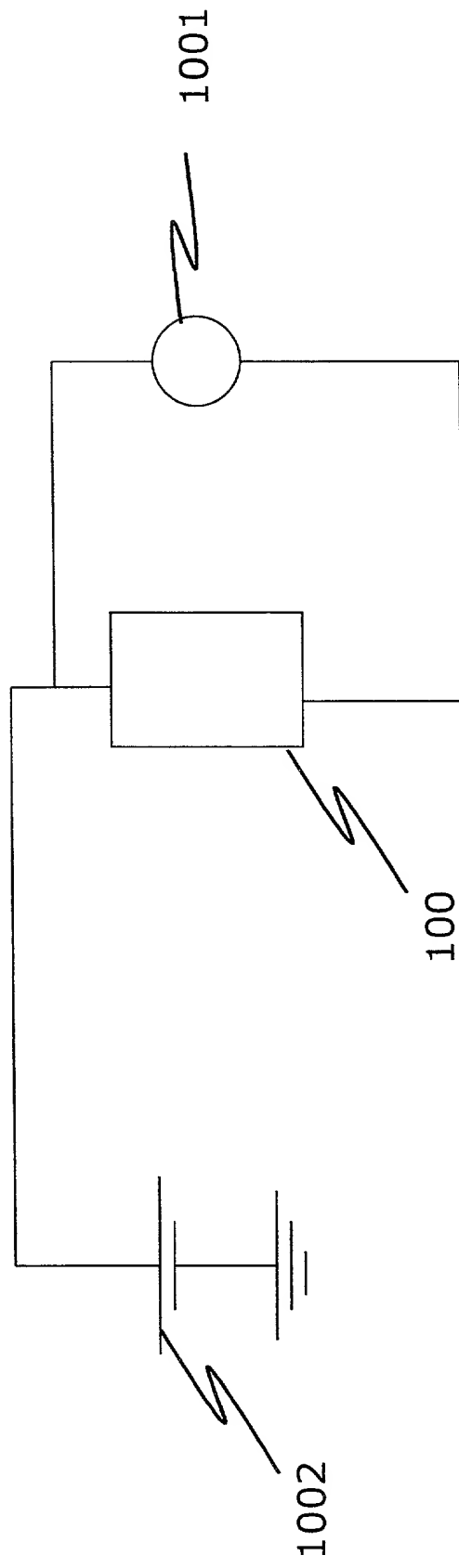


FIGURE 10